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## **An Introduction to Geotextiles in Erosion Control**

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*(Figures, tables and equations in this publication are at times a little difficult to read, but they are the best available. **DO NOT PURCHASE THIS PUBLICATION IF THIS LIMITATION IS UNACCEPTABLE TO YOU.**)*

**1. INTRODUCTION.** Erosion is caused by a group of physical and chemical processes by which the soil or rock material is loosened, detached, and transported from one place to another by running water, waves, wind, moving ice, or other geological sheet and bank erosion agents. Clayey soils are less erodible than fine sands and silts (see Fig. 1). This discussion covers the use of geotextiles to minimize erosion caused by water.

**2. BANK EROSION.** Riprap is used as a liner for ditches and channels subjected to high-velocity flow and for lake, reservoir and channel banks subject to wave action. Geotextiles are an effective and economical alternative to conventional graded filters under stone riprap. However, for aesthetic or economic reasons, articulated concrete mattresses, gabions, and precast cellular blocks have also been used to cover the geotextile. The velocity of the current, the height and frequency of waves and the erodibility of the bank determine whether bank protection is needed. The geotextiles used in bank protection serve as a filter.

### **2.1 SPECIAL DESIGN CONSIDERATIONS.**

**2.1.1 DURABILITY.** The term includes chemical, biological, thermal, and ultraviolet (UV) stability. Streams and runoff may contain materials that can be harmful to the geotextile. When protected from prolonged exposure to UV light, the common synthetic polymers do not deteriorate or rot in prolonged contact with moisture. All geotextile specifications must include a provision for covering the geotextile to limit its UV radiation exposure to 30 days or less.

**2.1.2 STRENGTH AND ABRASION RESISTANCE.** The required properties will depend on the specific application- the type of the cover material to be used (riprap, sand bags, concrete blocks, etc.), the size, weight, and shape of the armor stone, the handling placement techniques (drop height), and the severity of the conditions (stream velocity, wave height, rapid changes of water level, etc.). Abrasion can result from movement of the cover material as a result of wave action or currents. Strength properties generally considered of primary importance are tensile strength, dimensional stability, tearing, puncture, and burst resistance. Table 1 gives recommended minimum strength values.

**2.1.3 COVER MATERIAL.** The cover material (gravel, rock fragments, riprap, armor stone, concrete blocks, etc.) is a protective covering over the geotextile that minimizes or dissipates the hydraulic forces, protects the geotextile from extended exposure to UV radiation, and keeps it in intimate contact with the soil. The type, size, and weight of cover material placed over the geotextile depends on the kinetic energy of water. Cover material that is lightweight in comparison with the hydraulic forces acting on it may be moved. By removing the weight holding the geotextile down, the ground-water pressure may be able to separate the geotextile from the soil. When no longer constrained, the soil erodes. The cover material must be at least as permeable as the geotextile. If the cover material is not permeable enough, a layer of fine aggregate (sand, gravel, or crushed stone) should be placed between it and the geotextile. An important consideration in designing cover material is to keep the void area between stones relatively small. If the void area is excessively large, soils may move from areas weighted by stones to unweighted void areas between the stones, causing the geotextile to balloon or eventually rupture. The solution in this case is to place a graded layer of smaller stones below the large stones that will prevent the soil from moving. A layer of aggregate may also be needed if a major part of the geotextile is covered, as for example, by concrete blocks. The layer will act as a pore water dissipator.

**2.1.4 ANCHORAGE.** At the toe of the streambank, the geotextile and cover material should be placed along the bank to an elevation below mean low water level to minimize erosion at the toe. Placement to a vertical distance of 3 feet below mean low water level, or to the bottom of the streambed for streams shallower than 3 feet, is recommended. At the top of the bank, the geotextile and cover material should either be placed along the top of the bank or with 2 feet vertical freeboard above expected maximum water stage. If strong water movements are expected, the geotextile needs to be anchored at the crest and toe of the streambank (see Fig. 2).

**2.1.5 IF THE GEOTEXTILE** must be placed below low water, a material of a density greater than that of water should be selected.

Type	Strength Test Method	Class A <sup>1</sup>	Class B <sup>2</sup>
Grab Tensile	ASTM D 4632	200	90
Elongation (%)	ASTM D 4632	15	15
Puncture	ASTM D 4833	80	40
Tear	ASTM D 4533	50	30
Abrasion	ASTM D 3884	55	25
Seam	ASTM D 4632	180	80
Burst	ASTM D 3786	320	140

<sup>1</sup> Fabrics are used under conditions more severe than Class B such as drop height less than 3 feet and stone weights should not exceed 250 pounds.

Table 1

Recommended Geotextile Minimum Strength Requirements.

## 2.2 CONSTRUCTION CONSIDERATIONS.

**2.2.1 SITE PREPARATION.** The surface should be cleared of vegetation, large stones, limbs, stumps, trees, brush, roots, and other debris and then graded to a relatively smooth plane free of obstructions, depressions, and soft pockets of materials.

**2.2.2 PLACEMENT OF GEOTEXTILES.** The geotextile is unrolled directly on the smoothly graded soil surface. It should not be left exposed to UV deterioration for more than 1 week in case of untreated geotextiles, and for more than 30 days in case of UV protected and low UV susceptible polymer geotextiles. The geotextile should be loosely laid, free of tension, folds, and wrinkles. When used for streambank protection, where currents acting parallel to the bank are the principal erosion forces, the geotextile should be placed with the longer dimension (machine direction) in the direction of anticipated water flow. The upper strips of the geotextile should overlap the lower strips (see Fig. 3). When used for wave attack or cut and fill slope protection, the geotextile should be

placed vertically down the slope (see Fig. 3), and the upslope strips should cover the downslope strips. Stagger the overlaps at the ends of the strips at least 5 feet. The geotextile should be anchored at its terminal ends to prevent uplift or undermining. For this purpose, key trenches and aprons are used at the crest and toe of the slope.

**2.2.3 OVERLAPS, SEAMS, SECURING PINS.** Adjacent geotextile strips should have a minimum overlap of 12 inches along the edges and at the end of rolls. For underwater placement, minimum overlap should be 3 feet. Specific applications may require additional overlaps.

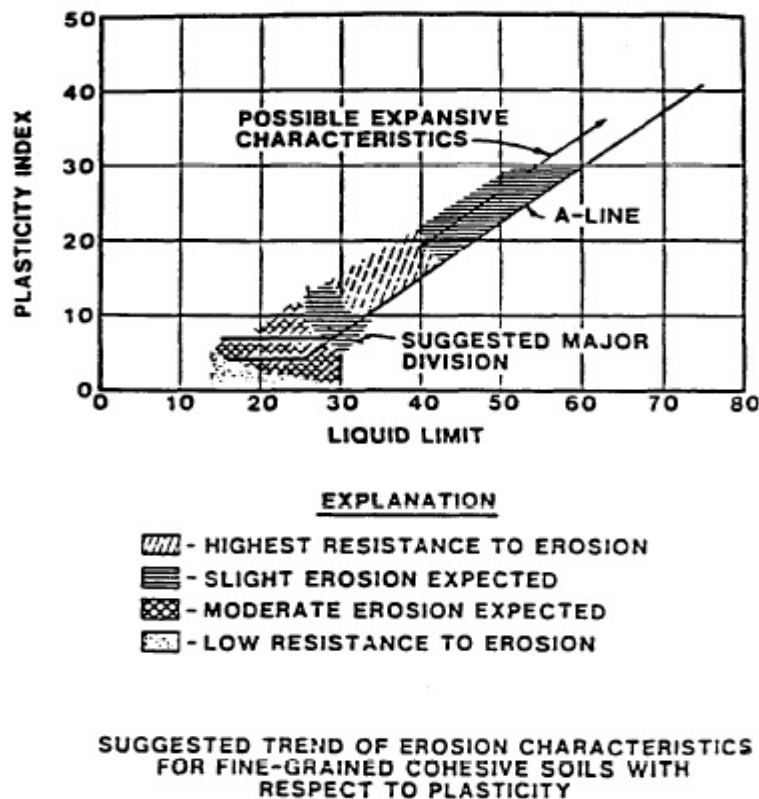


Figure 1  
Relationship between Atterberg Limits and Expected Erosion Potential.



Slope	Pin Spacing feet
Steeper than 1V on 3H	2
1V on 3H to 1V on 4H	3
Flatter than 1V on 4H	5

V = vertical; H = horizontal.

Table 2  
Pin Spacing Requirements in Erosion Control Applications

Sewing, stapling, heat, welding or gluing adjacent panels, either in the factory or on site, are preferred to lapping only. Sewing has proved to be the most reliable method of joining adjacent panels. It should be performed using polyester, polypropylene, kevlar or nylon thread. The seam strength for both factory and field seams should not be less than 90 percent of the required tensile strength of the unaged geotextile in any principal direction. Geotextiles may be held in place on the slope with securing pins prior to placing the cover material. These pins with washers should be inserted through both strips of the overlapped geotextile along a line through the midpoint of the overlap. The pin spacing, both along the overlaps or seams, depends on the slope as specified in Table 2. Steel securing pins, 3/16 inch in diameter, 18 inches long, pointed at one end, and fitted with a 1.5-inch metal washer on the other have performed well in rather firm soils. Longer pins are advisable for use in loose soils. The maximum slope on which geotextiles may be placed will be determined by the friction angles between the natural-ground and geotextile and cover- material and geotextile. The maximum allowable slope in no case can be greater than the lowest friction angle between these two materials and the geotextile.

**2.2.4 PLACEMENT OF COVER MATERIAL ON GEOTEXTILE.** For sloped surfaces, placement of the cover stone or riprap should start from the base of the slope moving upward and preferably from the center outward to limit any partial movement of soil because of sliding. In no case should drop heights which damage the geotextile be permitted. Testing may be necessary to establish an acceptable drop height.

### **3. PRECIPITATION RUNOFF COLLECTION AND DIVERSION DITCHES.**

A diversion ditch is an open, artificial, gravity flow channel which intercepts and collects precipitation runoff, diverts it away from vulnerable areas, and directs it toward stabilized outlets. A geotextile or revegetation mat can be used to line the ditch. It will retard erosion in the ditch, while allowing grass or other protective vegetation growth to take place. The mat or geotextile can serve as additional root anchoring for some time after plant cover has established itself if UV resistant geotextiles are specified. Some materials used for this purpose are designed to degrade after grass growth takes place. The geotextile can be selected and specified using physical properties indicated in Table 1. Figure 4 shows a typical example.

#### 4. MISCELLANEOUS EROSION CONTROL.

Figures 5 and 6 show examples of geotextile applications in erosion control at drop inlets and culvert outlets, and scour protection around bridges, piers and abutments. Design criteria similar to that used for bank protection should be used for these applications.

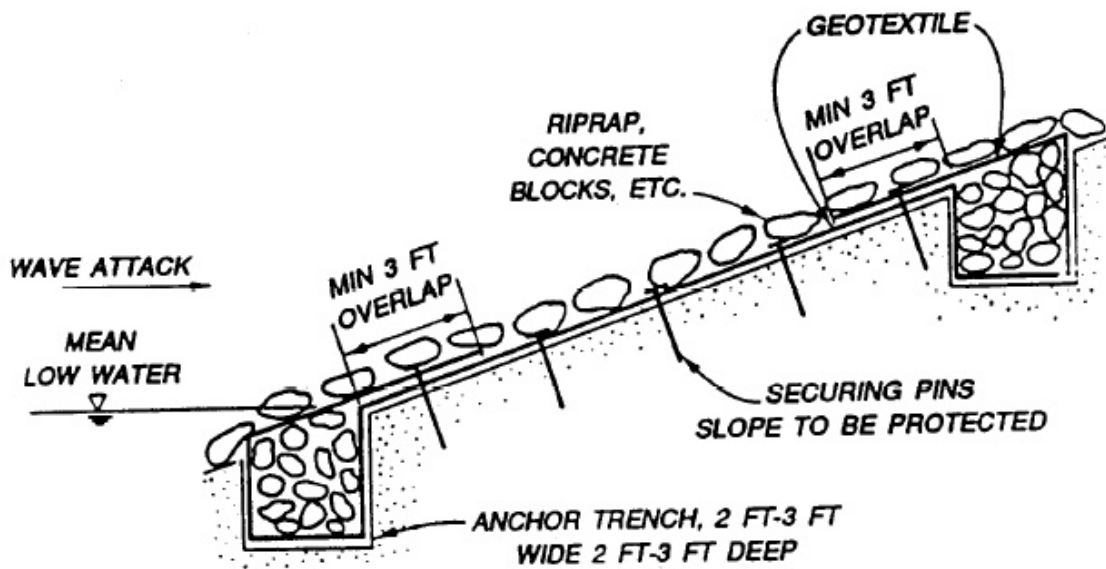


Figure 2

Pin Spacing Requirements in Erosion Control Applications.

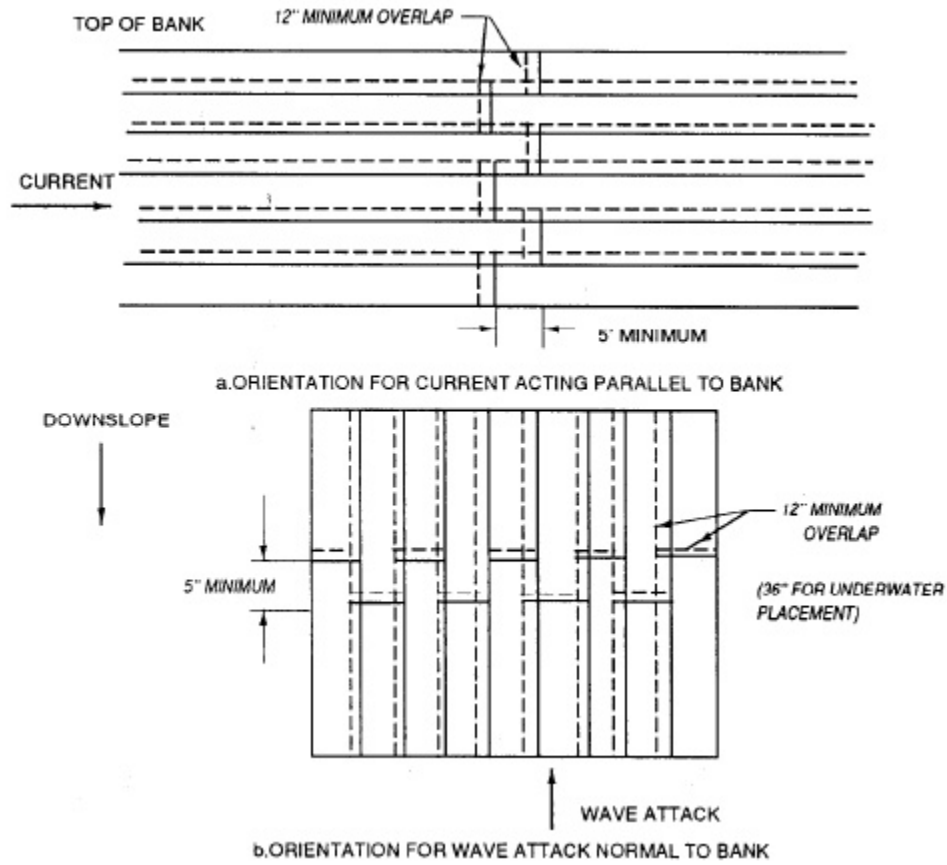


Figure 3  
Geotextile Placement for Currents Acting Parallel to Bank  
or for Wave Attack on the Bank.

**5. SEDIMENT CONTROL.** Silt fences and silt curtains are sediment control systems using geotextiles.

**5.1 SILT FENCE.** A silt fence is a temporary vertical barrier composed of a sheet of geotextile supported by fencing or simply by posts, as illustrated in Figure 5. The lower end of the geotextile is buried in a trench cut into the ground so that runoff will not flow beneath the fence. The purpose of the permeable geotextile silt fence is to intercept and detain sediment from unprotected areas before it leaves the construction site. Silt fence are sometimes located around the entire downslope portion or perimeter of urban construction sites. Short fences are often placed across small drainage ditches (permanent or temporary) constructed on the site. Both applications are intended to function for one or two construction seasons or until grass sod is established. The fence reduces water velocity allowing the sediment to settle out of suspension.

**5.1.1 DESIGN CONCEPTS.** A silt fence consists of a sheet of geotextile and a support component. The support component may be a wire or plastic mesh support fence attached to support posts or, in some cases, may be support posts only. The designer has to determine the minimum height of silt fences, and consider the geotextile properties (tensile strength, permeability) and external factors (the slope of the surface, the volume of water and suspended particles which are delivered to the silt fence, and the size of distribution of the suspended particles). Referring to Figures 6 and 7, the total height of the silt fence must be greater than  $h_1 + h_2 + h$ ; where  $h_1$  is the height of geotextile necessary to allow water flowing into the basin to flow through the geotextile, considering the permeability of the geotextile; and  $h_2$  is the height of water necessary to overcome the threshold gradient of the geotextile and to initiate flow. For most expected conditions,  $h_1 + h_2$  is about 6 inches or less. The silt fence accomplishes its purpose by creating a pond of relatively still water which serves as a sedimentation basin and collects the suspended solids from the runoff. The useful life of the silt fence is the time required to fill the triangular area of height

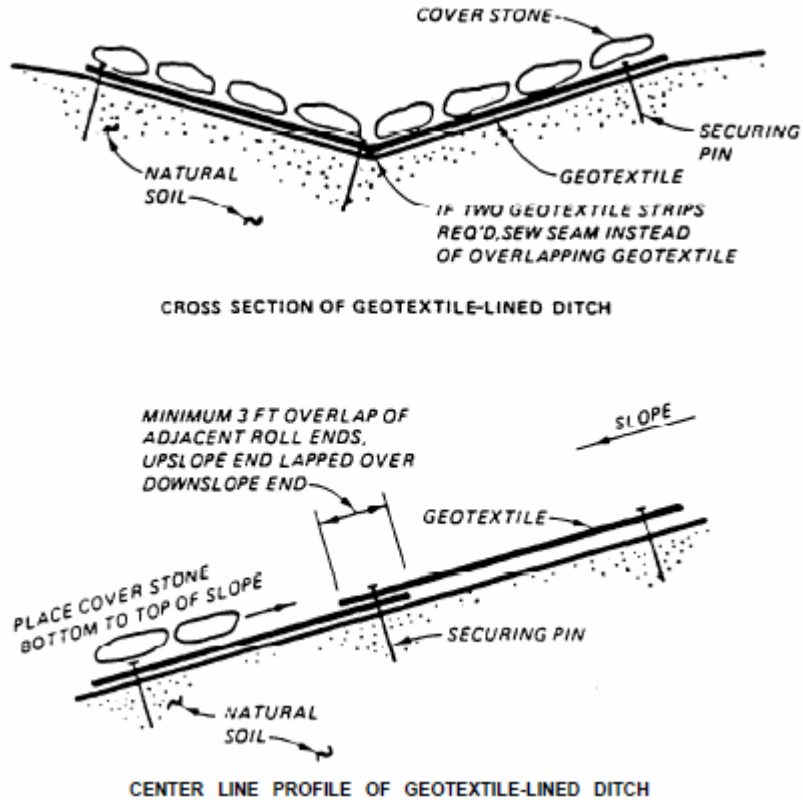


Figure 4  
Ditch liners

h (Fig. 7) behind the silt fence with sediment. The height of the silt fence geotextile should not exceed 3 feet.

**5.1.2 DESIGN FOR MAXIMUM PARTICLE RETENTION.** Geotextiles selected for use in silt fences should have an AOS that will satisfy the following equation with a limiting value equal to the No. 120 sieve size.

$$\frac{D^{85} \text{ (mm) (soil)}}{\text{AOS (mm) (geotextile)}} \geq 1 \quad (\text{Eq. 1})$$

A minimum of 90-pound tensile strength (ASTM D 4632 Grab Test Method) is recommended for use with support posts spaced a maximum of 8 feet apart.

**5.1.3 DESIGN FOR FILTRATION EFFICIENCY.** The geotextile should be capable of filtering most of the soil particles carried in the runoff from a construction site without unduly impeding the flow. ASTM D 5141 presents the laboratory test used to determine the filtering efficiency and the flow rate of the sediment-filled water through the geotextile.

**5.1.4 REQUIRED GEOTEXTILE PROPERTIES.** The geotextile used for silt fence must also have:

(a) Reasonable puncture and tear resistance to prevent damage by floating debris and to limit tearing where attached to posts and fence.

(b) Adequate resistance to UV deterioration and biological, chemical and thermal actions for the desired life of the fence.

**5.1.5 CONSTRUCTION CONSIDERATIONS.**

(a) Silt fences should be constructed after the cutting of trees but before having any sod disturbing construction activity in the drainage area.

(b) It is a good practice to construct the silt fence across a flat area in the form of a horseshoe. This aids in the ponding of the runoff, and increases the strength of the fence. Prefabricated silt fence sections containing geotextile and support posts are commercially available. They are generally manufactured in heights of 18 and 36 inches. At the lower portion of the silt fence, the geotextile is extended for burying anchorage.

**5.2 SILT CURTAINS.** A silt curtain is a floating vertical barrier placed within a stream, lake, or other body of water generally at runoff discharge points. It acts as a temporary dike to arrest and control turbidity. By interrupting the flow of water, it retains suspended particles; by reducing the velocity, it allows sedimentation. A silt curtain is composed of a sheet of geotextile maintained in a vertical position by flotation segments at the top and a ballast chain along the bottom. A tension cable is often built into the curtain



immediately above or below the flotation segments to absorb stress imposed by currents and other hydrodynamic forces. Silt curtain sections are usually about 100 feet long and of any required width. An end connector is provided at each end of the section for fastening sections together. Anchor lines hold the curtain in a configuration that is usually U-shaped, circular, or elliptical. The design criteria and properties required for silt fences also apply to silt curtains. Silt curtains should not be used for:

- (1) Operations in open ocean.
- (2) Operations in currents exceeding 1 knot.
- (3) Areas frequently exposed to high winds and large breaking waves.
- (4) Around hopper or cutterhead dredges where frequent curtain movement would be necessary.

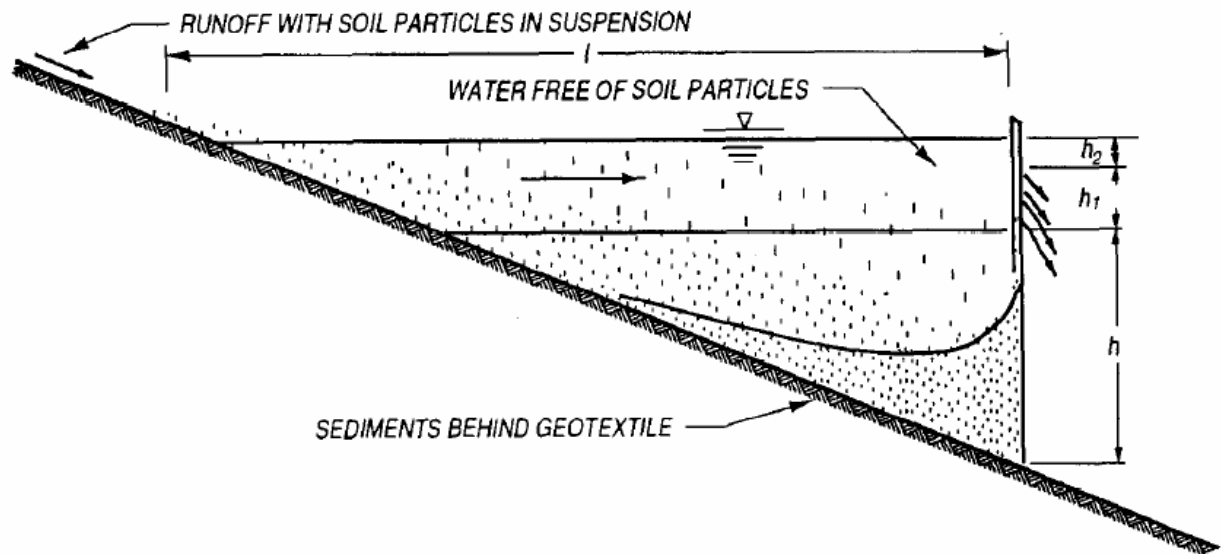


Figure 5  
Use of Geotextiles near Small Hydraulic Structures

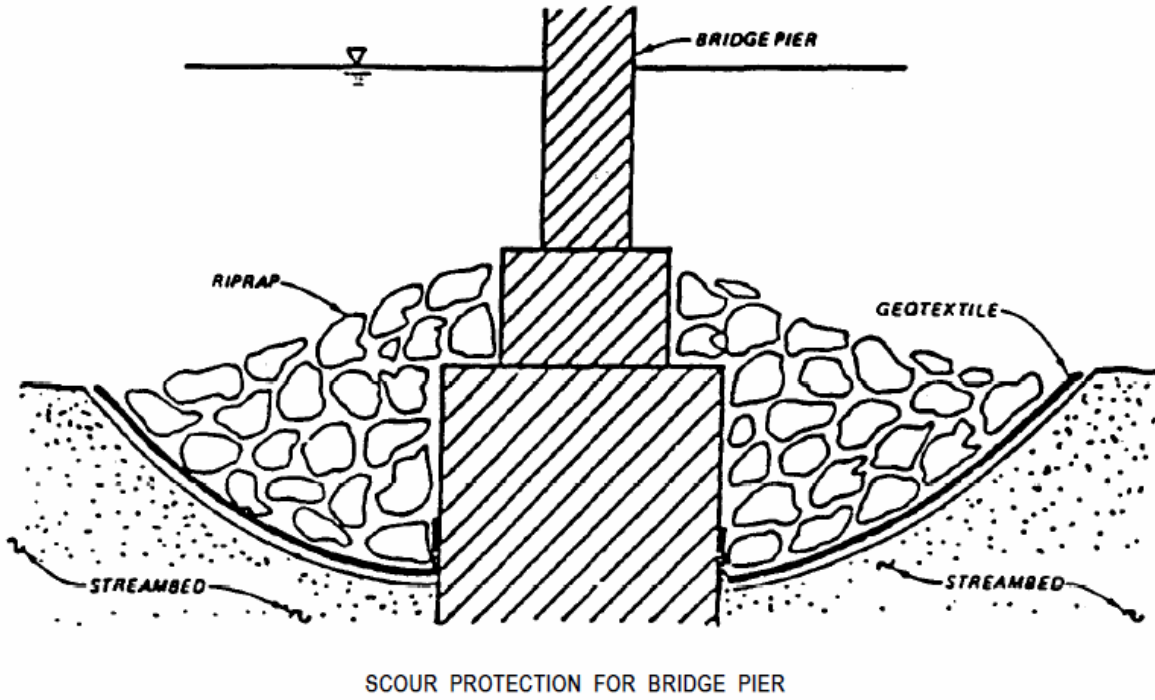


Figure 6  
Use of Geotextiles around Piers and Abutments

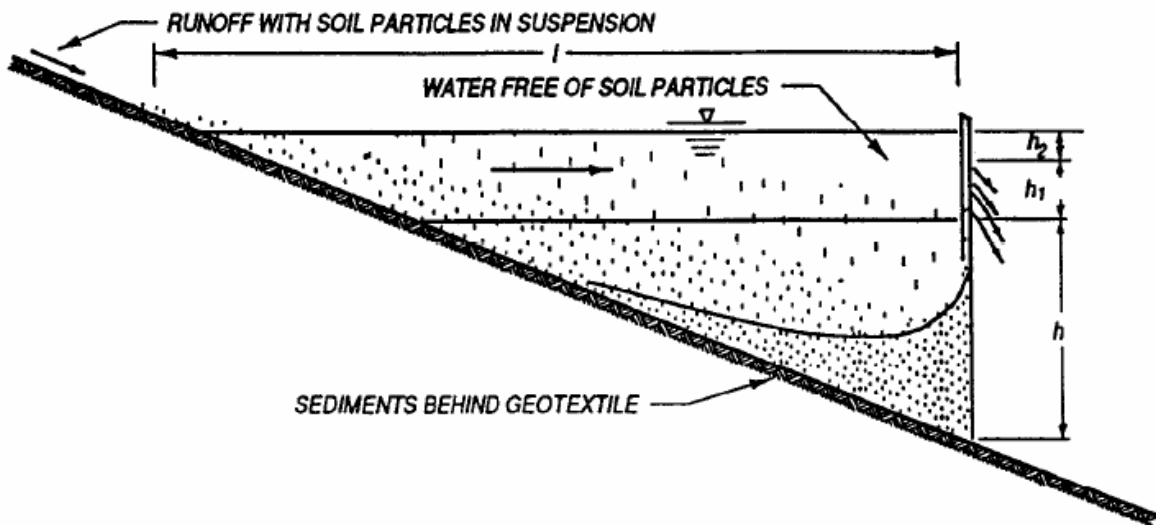


Figure 7  
Sedimentation behind Silt Fence.

## 6. REFERENCES

Al-Hussaini, M. M., "Field Experiment of Fabric Reinforced Earth Wall," *Proceedings of the International Conference on the Use of Fabrics in Geotechnics*, Paris, Apr 20-22, Vol. 1, pp. 119-121, 1977.

Al-Hussaini, M., and Perry, E. B., "Analysis of A Rubber- Membrane Strip Reinforced Earth Wall," *Soil Reinforcing and Stabilizing Techniques in Engineering Practice, Proceedings of a Symposium Jointly Organized by the New South Wales Institute of Technology and the University of New South Wales*, Sydney, Australia, 1978.

Andrawes, K. Z., McGowan, A., Wilson-Fahmy, R. F., and Mashhour, M. M., "The Finite-Element Method of Analysis Applied to Soil-Geotextile Systems," *Proceedings of the 2nd International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3, pp. 695-700, 1982.

Baker, R., "Tensile Strength, Tension Cracks and Stability of Slopes," *Soils and Foundations, Journal of the Japanese Society of Soil Mechanics and Foundations Engineering*, Vol. 21, No. 2, pp. 1-17, 1981.

Baker, R., and Garber, M., "Variational Approach to Slope Stability," *Proceedings of the 9th International Conference on Soil Mechanics and Foundation Engineering*, Vol. 2, pp. 9-12, Tokyo, 1977.

Baker, R., and Garber, M., "Theoretical Analysis of the Stability of Slopes," *Geotechnique*, Vol. 28, No. 4, pp. 395-411, 1978.

Barrett, R. K., "Geotextiles in Earth Reinforcement," *Geotechnical Fabrics Report*, Mar/Apr, Vol. 3, No. 2, pp. 15-99, 1988.

Bell, J. R., Barrett, R. K., and Ruckman, A. C., "Geotextile Earth-Reinforced Retaining Wall Tests: Glenwood Canyon, Colorado," *Transportation Research Record*, 916, pp. 59-69, 1983.

Bell, J. R., Greenway, D. R., and Vischer, W., "Construction and Analysis of a Fabric-Reinforced Low Embankment on Muskeg," *Proceedings, International Conference on the Use of Fabrics in Geotechniques*, Paris, Vol. 1, pp. 71-76, 1977.

Bell, J. R., and Hicks, R. G., "Evaluation of Test Methods and Use Criteria for Geotechnical Fabrics in Highway Applications, Final Report," Federal Highway Administration, Washington, DC, 1983.

Bell, J. R., and Steward, J. E., "Construction and Observation of Fabric Retained Soil Walls," *Proceedings of the International Conference on the Use of Fabrics in Geotechnics*, April 20-22, Vol. 1, pp. 123-128, 1977.

Bell, J. R., Stille, A. N., and Vandre, B., "Fabric Retained Earth Walls," *Proceedings of the 13th Annual Engineering Geology and Soils Engineering Symposium*, University of Idaho, Moscow, Idaho, April 2-4, pp. 271-287, 1975.

Blair, J. C., Bell, J. R., and Hicks, R. G., "Permeability Testing of Geotextiles," *Transportation Research Record*, 826, pp. 1-6, 1981.

Broms, B. B., "Design of Fabric Reinforced Retaining Structures," *Proceedings of the Symposium on Earth Reinforcement*, American Society of Civil Engineers, Pittsburgh, Penn., 1978.

Campbell, D. H., et al., "Erosion Objective: Storm Water Drainage Channel Needs Erosion Protection," *Geotechnical Fabrics Report*, p. 20, 1985.

Cedergren, H. R., *Seepage, Drainage, and Flownets*, Wiley, New York, 1977.

Chassie, R. G., "Geotextile Retaining Walls: Some Case History Examples," paper prepared for presentation at the 1984 NW Roads and Streets Conference, Corvallis, Oreg., 1984.

Chen, W. F., *Limit Analysis and Soil Plasticity*, Elsevier Pub., Amsterdam, The Netherlands, 1975.

Christie, I. F., and E-Hadi, K. M., "Some Aspects of the Design of Earth Dams Reinforced with Fabric," *Proceedings of the International Conference on the Use of Fabrics in Geotechnics*, Paris, April 20-22, Vol. 1, pp. 99-103, 1977.

Christopher, B. R. 1983. "Evaluation of Two Geotextile Installations in Excess of a Decade Old," *Transportation Research Record* 916, National Academy of Sciences, Washington, DC, p 79-88.

Christopher, B. R., and Holtz, R. D., "Geotextile Engineering Manual," Report No. FHWA-TS-861203, STS Consultants Ltd, Northbrook, Ill under contract FHWA No. DTFH61-83-C-00094, 1984.

Civil Works Construction Guide Specification, No. CW 02215, "Plastic Filter Fabric," Department of the Army Corps of Engineers, Office of the Chief of Engineers, Washington, DC, 1986.

Couch, F. B., Jr., "Geotextile Applications to Slope Protection for the Tennessee-Tombigbee Waterway Divide Cut," Second International Conference on Geotextiles, Las Vegas, Nev., 1982.

Coutermarsh, B. A. and G. Phetteplace, "Numerical Analysis of Frost Shields," in *Proceedings, American Society of Civil Engineers/Canadian Geotechnical Society Sixth International Cold Regions Specialty Conference*, W. Lebanon, NH, February 26-28, 1991, p. 178-190.

Coutermarsh, B. A. and G. Phetteplace, “*Analysis of Frost Shields Using the Finite Element Method*,” Seventh International Conference on Numerical Methods in Thermal Problems, Stanford, CA, Pineridge Press, Swansea, UK, p. 123-132.

De Ment, L. E., “Two New Methods of Erosion Protection for Louisiana,” *Shore Beach*, Vol. 45, No. 1, p. 8, 1977.

Douglas, G. E., “Design and Construction of Fabric-Reinforced Retaining Walls by New York State,” *Transportation Research Record*, 872, pp. 32-37, 1982.

El-Fermaoui, A., and Nowatzki, E., “Effect of Confining Pressure on Performance of Geotextiles in Soils,” *Proceedings of the 2nd International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3, pp. 799-804, 1982.

Engineering and Design, “Use of Geotextiles Under Riprap,” Engineer Technical Letter No. 1110-2-286, Department of the Army, US Army Corps of Engineers, Washington, DC, 1984.

Ford, H. W., “Estimating the Potential for Ochre Clogging Before Installing Drains,” *Transactions of the American Society of Civil Engineers* 25(6), pp. 1597-1600, 1982a.

Ford, H. W., “Some Fundamentals of Iron and Slime Deposition in Drains,” *Proceedings of the Second International Drainage Workshop*, Washington, DC, pp. 207-212, 1982b.

Fowler, Jack, “Analysis of Fabric-Reinforced Embankment Test Section at Pinto Pass, Mobile, Alabama,” thesis submitted in partial fulfillment of the requirements for the degree of Doctor of Philosophy, Oklahoma State University, Stillwater, Okla., 1979.

Fowler, J., “Theoretical Design Considerations for Fabric-Reinforced Embankments,” *Proceedings of the 2nd International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3, pp. 665-670, 1982.

*Geotextiles and Geomembranes*, T. S. Ingold, Ed., published by Elsevier Applied Science Publishers, Essex, England, containing articles on geotextiles and geomembranes, began publication in 1984.

*Geotechnical Fabrics Report*, Published by Industrial Fabrics Association International since 1981, St. Paul, Minn.

Giroud, J. P., “Filter Criteria for Geotextiles,” *Proceedings of the Second International Conference on Geotextiles*, Vol. I, pp. 103-108, 1982.

Gulden, W., and Brown, D., “Treatments for Reduction of Reflective Cracking of Asphalt Overlays on Jointed-Concrete Pavements in Georgia,” *Transportation Research Record* 916, Transportation Research Board, Washington, DC, 1983.

Haliburton, T. A., “Design of Test Section for Pinto Pass Dike, Mobile, Alabama,” Report prepared by Haliburton Associates, Stillwater, Okla., under Contract No. DACW01-78-C-0092, for US Army Engineer District, Mobile, Ala., 1978.

Haliburton, T. A., "Evaluation of Construction Procedure for Fabric-Reinforced Embankment Test Section, Pinto Pass, Mobile Harbor, Alabama," conducted by Haliburton Associates, Stillwater, Okla., under Contract No. DACW39-78-M-4002, for US Army Engineer Waterways Experiment Station, Vicksburg, Miss., 1979.

Haliburton, T. A., Anglin, C. C., and Lawmaster, J. D., "Selection of Geotechnical Fabrics for Embankment Reinforcement," School of Civil Engineering, Oklahoma State University, Stillwater, Okla., 1978.

Haliburton, T. A., Fowler, J., and Langan, J. P., "Design and Construction of Fabric-Reinforced Embankment Test Section at Pinto Pass, Mobile, Alabama," *Transportation Research Record*, 249, pp. 27-34, Washington, DC, 1980.

Haliburton, T. A., Lawmaster, J. D., and King, J. J., "Potential Use of Geotechnical Fabric in Airfield Runway Design," Contract No. AFOSR79-00871, Air Force Office of Scientific Research, School of Civil Engineering, Oklahoma State University, Stillwater, Okla., 1980.

Haliburton, T. A., Lawmaster, J. D., and McGuffie, V. C., "Use of Engineering Fabrics in Transportation Related Applications," Haliburton Associates Engineering Consultants, Under Contract No. DTFH-80-C-0094, Stillwater, Okla., 1981.

Hammer, D. P., and Blackburn, E. D., "Design and Construction of Retaining Dikes for Containment of Dredged Material," Technical Report TR-D-77-9, US Army Engineer District, Savannah, Savannah, Ga., 1977.

Henry, K. S., "*Geotextiles as Capillary Barriers*," Geotechnical Fabrics Report, March/April, pp. 30-36.

Henry, K. S., "*Laboratory Investigation of the Use of Geotextiles to Mitigate Frost Heave*," CRREL Report 90-6, CRREL, Hanover, NH USA, 28 p.

Henry, K. S., "*Use of Geotextiles to Mitigate Frost Heave in Soils*," in Proceedings, V International Conference on Permafrost in Trondheim, Norway, Vol. 2, p. 1096-1011.

Henry, K. S., S. Taylor and J. Ingersoll, "*Effects of Freezing on the Microstructure of Two Geotextiles*," in Geosynthetics: Microstructure and Performance, ASTM STP 1076, pp. 147-164.

Henry, Karen S., "*Effect of Geotextiles on Water Migration in Freezing Soils and the Influence of Freezing on Performance*," Proceedings, Geosynthetics, 91, Atlanta, GA, Industrial Fabrics Association International, St. Paul, MN.

Horz, R. C., "Geotextiles for Drainage, Gas Venting, and Erosion Control at Hazardous Waste Sites," Report No. EPA/600/2-86/085, US Environmental Protection Agency, Cincinnati, Ohio, 1986.

Ingold, T. S., "An Analytical Study of Geotextile Reinforced Embankments," *Proceedings of the 2<sup>nd</sup> International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3, pp. 683-688, 1982.

Instruction for Use of Construction Specification No. 210, "Plastic Filter Cloth," Department of the Army Corps of Engineers, Office of the Chief of Engineers, Washington, DC, 1981.

Jewell, R. A., "A Limit Equilibrium Design Method for Reinforced Embankments of Soft Foundations," *Proceedings of the 2nd International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3.) pp. 671-676, 1982.

Jones, C. J. F. P., *Earth Reinforcement and Soil Structures*, Butterworth and Co., Ltd., London, 1985.

Keown, M. P., and Oswalt, N. R., "US Army Corps of Engineers Experience with Filter Fabric for Streambank Protection Applications, Flexible Armored Revetments Incorporating Geotextiles," *Proceedings of the International Conference Organized by the Institution of Civil Engineers*, London, 1984.

Koerner, R. M., *Designing with Geosynthetics*, Prentice-Hall, Englewood Cliffs, N.J., 1986.

Koerner, R. M., and Bove, J. A., "In-Plane Hydraulic Properties of Geotextiles," *Geotechnical Testing Journal*, Vol. 6, No. 4, pp. 190-195, 1983.

Koerner, R. M., and Welsh, J. P., *Construction and Geotechnical Engineering Using Synthetic Fabrics*, Wiley, New York, 1980.

Lamb, T. W., and Whitman, R. V., *Soil Mechanics, SI Version*, Wiley, New York, 1979.

Lee, K. L., Adams, B. D., and Vagneron, J-M. J., "Reinforced Earth Retaining Walls," *Journal of the Soil Mechanics and Foundations Division, American Society of Civil Engineers*, Vol. 99, No. SM10, pp. 745-764, 1973.

Leshchinsky, D., "Geotextile Reinforced Earth, Part I & II," Research Report Nos. CE 84-44/45, Department of Civil Engineering, University of Delaware, Newark, Del., 1984.

Leshchinsky, D., Baker, R., and Silver, M. L., "Three Dimensional Analysis of Slope Stability," *International Journal for Numerical and Analytical Methods in Geomechanics*, Vol. 9, pp. 199-223, 1985.

Leshchinsky, D., and Boedeker, R. H., "Geosynthetic Reinforced Soil Structures," *Journal of the Geotechnical Engineering*, American Society of Civil Engineers, Vol. 115, No. 10, pp. 1459-1478, 1989.

Leshchinsky, D., and Field, D. A., "In-Soil Load Elongation, Tensile Strength and Interface Friction of Nonwoven Geotextiles," *Proceedings of the Geosynthetics '87 Conference*, New Orleans, Feb 24-25, Vol. 1, pp. 238-249, 1987.

Leshchinsky, D., and Perry, E. B., "On the Design of Geosynthetic-Reinforced Walls," *Geotextiles and Geomembranes*, (in press), 1989.

Leshchinsky, D., and Reinschmidt, A. J., "Stability of Membrane Reinforced Slopes," *Journal of the Geotechnical Engineering, American Society of Civil Engineers*, Vol. 111, No. 11, pp. 1285-1300, 1985.

Leshchinsky, D., and Volk, J. C., "Stability Charts for Geotextile Reinforced Walls," *Transportation Research Record, 1031*, pp. 5-16, 1985.

McGhee, K. H., "Efforts to Reduce Reflective Cracking of Bituminous Concrete Overlays of Portland Cement Concrete Pavements," Virginia Highway and Transportation Research Council, Charlottesville, Va., 1975.

McGowan, A., Andrawes, K. Z., and Kabir, M. H., "Load-Extension Testing of Geotextiles Confined In-Soil," *Proceedings of the 2nd International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3, pp. 793-798, 1982.

Meyerhof, G. G., "The Bearing Capacity of Foundations Under Eccentric and Inclined Loads," *Proceedings, 34th International Conference on Soil Mechanics and Foundation Engineering*, Zurich, Vol. 1, pp. 440-445, 1953.

Mitchell, J. K., "Earth Walls," *Transportation News*, Transportation Research Board, National Research Council, No. 114, pp. 24-31, 1984.

Mohney, J., "Fabric Retaining Wall-Olympic N. F.," *Highway Focus*, Vol. 9, No. 1, pp. 88-103, 1977.

Murray, R. T., "Fabric Reinforced Earth Walls: Development of Design Equations," *Ground Engineering*, Vol. 13, No. 7, pp. 29-36, 1980.

Murray, R. T., "Fabric Reinforced Earth Walls: Development of Design Equations," Supplementary Report 496, Structures Department, Transport and Road Research Laboratory, Crowthorne, Berkshire, United Kingdom, 1981.

Murray, R., "Fabric Reinforcement of Embankments and Cuttings," *Proceedings of the 2nd International Conference on Geotextiles*, Las Vegas, Aug 1-6, Vol. 3, pp. 707-713, 1982.

Perloff, W. H., *Pressure Distribution and Settlement*, Chapter 4 in *Foundation Engineering Handbook*, ed. by Winterkorn and Fang, Van Nostrand Reinhold Company, New York, 1975.

Perloff, W. H., and Baron, W., *Soil Mechanics: Principles and Applications*, Wiley, 1976.  
*Proceedings, International Conference on the Use of Fabrics in Geotechnics*, Ecole Nationale des Ponts et Chaussees, Paris, 3 Vol., 1977.



*Proceedings of the First Canadian Symposium on Geotextiles* (Calgary, Canada, Sep 1980), published by the Canadian Geotechnical Society, 700 EIC Bldg, 2050 Mansfield St., Montreal, Quebec, Canada, 1980.

*Proceedings, Second International Conference on Geotextiles*, Industrial Fabrics Association International, St. Paul, Minn., 4 Vol., 1982.

Rankilor, P. R., *Membranes in Ground Engineering*, Wiley, Chichester, United Kingdom, 1981.

Raymond, G. P., "Installation Factors that Affect Performance of Railroad Geotextiles," *Transportation Research Record 1071*, Transportation Research Board, Washington, DC, 1986.

Richards, D. L., and Middleton, L. M., "Best Management Practices for Erosion and Sediment Control," Federal Highway Administration, Arlington, Va., 1978.

Risseeuw, Ir. P., "Stabilenka Woven Reinforcement Fabric in Raising Mounds on Soft Soil," Report NO. R.O. 5300.005, Akzo Research Laboratories, Department, C.T.I., Arnhem, The Netherlands, 1977.

Rowe, R. K., "Reinforced Embankments: Analysis and Design," *Journal of the Geotechnical Engineering, American Society of Civil Engineers*, Vol. 110, No. 2, pp. 231-246, 1984.

Sherard, J. L., "Sinkholes in Dams of Coarse, Broadly Graded Soils," *Thirteenth Conference of the International Congress on Large Dams*, New Delhi, India, Vol. 2, pp. 25-35, 1979.

Shoop, S. A. and K. Henry, "*The Effect of a Geotextile on Water Migration and Frost Heave in Large-Scale Tests*," preprint 910532, Transportation Research Board, 70th Annual Meeting, January 13-17, 1991.

Spangler, M. G., *Soil Engineering*, International Textbook Company, New York, 1951.

Stilley, A. N., "A Model Study of Fabric Reinforced Earth Walls," thesis submitted in partial fulfillment of the requirements for the Degree of Master of Science to Oregon State University, Corvallis, Oreg., 64 pp., 1974.

Terzaghi, K., and Peck, R. B., *Soil Mechanics in Engineering Practice*, 2nd Ed., Wiley, New York, 1967.

US Department of Transportation, "Sample Specifications for Engineering Fabrics," FHWA Report TS-78-211, Federal Highway Administration, Washington, DC, 1978.

Van Zanten, R. V., *Geotextiles and Geomembranes in Civil Engineering*, A. A. Balkema, Rotterdam, The Netherlands, 1986.

Volk, J. C., "Analysis and Design of Geotextile Reinforced Walls," thesis submitted in partial fulfillment of the requirements for the Degree of Master of Civil Engineering to the Faculty of the University of Delaware, Newark, Del., 1984.

Weimar, R. D., Jr., "Mechanism of the Geotextile Performance in Soil-Fabric Systems for Drainage and Erosion Control," *Transportation Research Record No. 916*, pp. 37-40, Transportation Research Board, 1983.

Winterkorn, H. F., and Fang, H-Y, *Foundation Engineering Handbook*, Van Nostrand Reinhold Company, New York, 1975.

Wyant, David C., "Evaluation of Filter Fabrics for Use as Silt Fences," Report No. VHTRC 80-R49, Virginia Highway and Transportation Research Council, Charlottesville, Va., 1980.